

Appendix 6. Location, physical characteristics, borehole-geophysical logs and interpreted structures for well Gates 1.

The Gates Pond Site is located in Berlin, MA along I-495. There are four wells. The wells are approximately ± 100 meters away from Gates Pond, which is the Town of Hudson, MA. The Town of Hudson commissioned the drilling of the wells in attempt to find a clean and sustainable groundwater source to augment their surface supplies. No such source was found so all four wells remain open. The wells produced five gallons per minute or less based on drillers pumping tests. Three wells were investigated for this study. They are named gates1.051507, gates2.062607 and gates3.071807.

The overburden material at the site is glacial till, with thicknesses less than 3 meters. The till is composed of a nonsorted, nonstratified matrix of sand with some clay, silt and boulders. The bedrock is schist of the Nashoba Formation. The Nashoba is a fine to medium grained, and well foliated, gray to silvery-gray quartz-mica schist that may contain biotite, garnet and sillimanite. All wells are cased approximately four meters into the bedrock.

The well gates1.051507 was the first well logged in this study. It was logged from May 15 through 18, 2007. Heat pulse flow meter tests were run on June 21, 2007. The well is reported to be 265 meters deep; however it was found to be only 179 meters deep. It is possible that the lower 90 meters collapsed in the year between drilling and logging or the well has become otherwise obstructed. The well casing was approximately 7.3 meters in length with about 3 meters of glacial overburden. A total of 255 fractures were identified in this well. Of the total fractures 166 are tectonic joints, 26 are subhorizontal unloading joints and 63 are FPF.

The water table in the well was approximately 5.7 meters below ground surface. For the heat pulse flow meter testing, the well was pumped for three hours during which time the water level was drawn down 0.07 meters. Heat pulse flow meter testing revealed five flowing fractures at 19.0, 21.7, 25.0, 73.7, and 106.4 meters depth. Of the flowing fractures two are FPF, two are tectonic joints and one is subhorizontal.

Appendix 6, continued. Midpoint depth, strike and dip of features identified in optical televiewer log, fracture type and heat pulse flowmeter data from Gates 1 (azimuth and dip reported using right hand rule convention; t = tectonic fractures, s = sheeting joints, p = foliation parallel fractures). Flow data shown under pumping conditions have been normalized.

Site ID: gates1.051507
 Location: "Gates Pond I" Berlin, MA

Elevation (m) 90
 Reported Yield (gpm) 5
 Rock Type: Nashoba Formation Schist

Depth to water: 18.67 ft 5.69 m
 Depth of casing: 24 ft 7.32 m
 Depth of well: 588 ft 179.22 m
 Land surface to MP: 2.25 ft 0.69 m

| number | Fractures | | | | | Ambient | | | Pump at 0.5 gpm | | |
|--------|-----------|------------|---------|-----|------|------------|-------|---------|-----------------|-------|---------|
| | depth (m) | depth (ft) | Azimuth | Dip | Type | Flow (y/n) | gpm | notes | Flow (y/n) | gpm | notes |
| 1 | 7.70 | 25.3 | 247 | 60 | p | n | 0 | | n | 0.50 | |
| 2 | 7.84 | 25.7 | 186 | 58 | p | n | 0 | | n | 0.50 | |
| 3 | 8.00 | 26.3 | 192 | 30 | p | n | 0 | | n | 0.50 | |
| 4 | 8.10 | 26.6 | 93 | 85 | t | n | 0 | | n | 0.50 | |
| 5 | 9.71 | 31.9 | 22 | 20 | s | n | 0 | | n | 0.50 | |
| 6 | 9.79 | 32.1 | 260 | 10 | s | n | 0 | | n | 0.50 | |
| 7 | 10.12 | 33.2 | 140 | 59 | t | n | 0 | | n | 0.50 | |
| 8 | 10.16 | 33.3 | 118 | 78 | t | n | 0 | | n | 0.50 | |
| 9 | 10.19 | 33.4 | 132 | 58 | t | n | 0 | | n | 0.50 | |
| 10 | 10.67 | 35.0 | 252 | 29 | p | n | 0 | | n | 0.50 | |
| 11 | 10.83 | 35.5 | 334 | 70 | t | n | 0 | | n | 0.50 | |
| 12 | 11.20 | 36.8 | 317 | 68 | t | n | 0 | | n | 0.50 | |
| 13 | 12.18 | 40.0 | 88 | 75 | t | n | 0 | | n | 0.50 | |
| 14 | 13.36 | 43.8 | 73 | 69 | t | n | 0 | | n | 0.50 | |
| 15 | 13.96 | 45.8 | 238 | 73 | p | n | 0 | | n | 0.50 | |
| 16 | 14.10 | 46.3 | 247 | 80 | p | n | 0 | | n | 0.50 | |
| 17 | 14.49 | 47.6 | 84 | 24 | s | n | 0 | | n | 0.50 | |
| 18 | 14.98 | 49.2 | 189 | 69 | p | n | 0 | | n | 0.50 | |
| 19 | 15.34 | 50.3 | 199 | 70 | p | n | 0 | | n | 0.50 | |
| 20 | 15.67 | 51.4 | 21 | 79 | p | n | 0 | | n | 0.50 | |
| 21 | 15.71 | 51.5 | 187 | 70 | p | y | -0.03 | flow in | n | 0.50 | |
| 22 | 15.93 | 52.3 | 186 | 76 | p | n | -0.03 | | n | 0.50 | |
| 23 | 16.36 | 53.7 | 190 | 71 | p | n | -0.03 | | n | 0.50 | |
| 24 | 17.04 | 55.9 | 40 | 75 | t | n | -0.03 | | n | 0.50 | |
| 25 | 17.61 | 57.8 | 71 | 72 | t | n | -0.03 | | n | 0.50 | |
| 26 | 18.36 | 60.2 | 140 | 11 | s | n | -0.03 | | n | 0.50 | |
| 27 | 18.96 | 62.2 | 256 | 57 | p | n | -0.03 | | n | 0.50 | |
| 28 | 19.03 | 62.5 | 260 | 65 | p | n | -0.03 | | y | 0.50 | flow in |
| 29 | 19.10 | 62.7 | 261 | 67 | p | n | -0.03 | | n | 0.22 | |
| 30 | 19.31 | 63.4 | 265 | 70 | p | n | -0.03 | | n | 0.22 | |
| 31 | 19.65 | 64.5 | 262 | 72 | p | n | -0.03 | | n | 0.22 | |
| 32 | 19.74 | 64.8 | 265 | 75 | p | n | -0.03 | | n | 0.22 | |
| 33 | 20.20 | 66.3 | 116 | 30 | t | n | -0.03 | | n | 0.22 | |
| 34 | 20.26 | 66.5 | 222 | 74 | p | n | -0.03 | | n | 0.22 | |
| 35 | 21.00 | 68.9 | 77 | 64 | t | n | -0.03 | | n | 0.22 | |
| 36 | 21.01 | 68.9 | 349 | 61 | t | n | -0.03 | | n | 0.22 | |
| 37 | 21.23 | 69.7 | 97 | 32 | t | n | -0.03 | | n | 0.22 | |
| 38 | 21.43 | 70.3 | 348 | 35 | t | n | -0.03 | | n | 0.22 | |
| 39 | 21.73 | 71.3 | 7 | 55 | t | y | -0.17 | flow in | y | 0.22 | flow in |
| 40 | 22.27 | 73.1 | 193 | 70 | p | n | -0.17 | | n | 0.00 | |
| 41 | 22.87 | 75.0 | 193 | 78 | p | n | -0.17 | | n | 0.00 | |
| 42 | 22.96 | 75.3 | 6 | 25 | s | n | -0.17 | | n | 0.00 | |
| 43 | 23.72 | 77.8 | 272 | 85 | t | n | -0.17 | | n | 0.00 | |
| 44 | 24.09 | 79.0 | 17 | 72 | t | n | -0.17 | | n | 0.00 | |
| 45 | 25.00 | 82.0 | 323 | 47 | t | n | -0.17 | | n | 0.00 | |
| 46 | 25.05 | 82.2 | 331 | 45 | t | y | -0.3 | flow in | y | -0.09 | flow in |
| 47 | 25.87 | 84.9 | 336 | 45 | t | n | -0.3 | | n | -0.09 | |
| 48 | 25.96 | 85.2 | 315 | 50 | t | n | -0.3 | | n | -0.09 | |
| 49 | 27.73 | 91.0 | 111 | 76 | t | n | -0.3 | | n | -0.09 | |
| 50 | 28.94 | 94.9 | 156 | 39 | t | n | -0.3 | | n | -0.09 | |

Appendix 6, continued. Midpoint depth, strike and dip of features identified in optical televiewer log, fracture type and heat pulse flowmeter data from Gates 1 (azimuth and dip reported using right hand rule convention; t = tectonic fractures, s = sheeting joints, p = foliation parallel fractures). Flow data shown under pumping conditions have been normalized.

| | | | | | | | | | |
|-----|-------|-------|-----|----|---|---|------|---|-------|
| 51 | 29.81 | 97.8 | 335 | 57 | t | n | -0.3 | n | -0.09 |
| 52 | 30.51 | 100.1 | 317 | 64 | t | n | -0.3 | n | -0.09 |
| 53 | 30.74 | 100.9 | 137 | 70 | t | n | -0.3 | n | -0.09 |
| 54 | 31.65 | 103.8 | 280 | 62 | p | n | -0.3 | n | -0.09 |
| 55 | 32.67 | 107.2 | 295 | 68 | t | n | -0.3 | n | -0.09 |
| 56 | 32.86 | 107.8 | 285 | 72 | t | n | -0.3 | n | -0.09 |
| 57 | 32.97 | 108.2 | 292 | 73 | t | n | -0.3 | n | -0.09 |
| 58 | 33.49 | 109.9 | 292 | 66 | t | n | -0.3 | n | -0.09 |
| 59 | 34.29 | 112.5 | 281 | 77 | t | n | -0.3 | n | -0.09 |
| 60 | 34.54 | 113.3 | 320 | 10 | s | n | -0.3 | n | -0.09 |
| 61 | 34.56 | 113.4 | 267 | 70 | t | n | -0.3 | n | -0.09 |
| 62 | 35.25 | 115.7 | 280 | 66 | t | n | -0.3 | n | -0.09 |
| 63 | 35.28 | 115.8 | 286 | 64 | t | n | -0.3 | n | -0.09 |
| 64 | 35.37 | 116.1 | 59 | 28 | t | n | -0.3 | n | -0.09 |
| 65 | 35.47 | 116.4 | 90 | 37 | t | n | -0.3 | n | -0.09 |
| 66 | 35.87 | 117.7 | 265 | 65 | p | n | -0.3 | n | -0.09 |
| 67 | 35.90 | 117.8 | 297 | 74 | t | n | -0.3 | n | -0.09 |
| 68 | 36.13 | 118.5 | 285 | 72 | t | n | -0.3 | n | -0.09 |
| 69 | 36.74 | 120.6 | 87 | 7 | s | n | -0.3 | n | -0.09 |
| 70 | 37.13 | 121.8 | 273 | 64 | t | n | -0.3 | n | -0.09 |
| 71 | 37.57 | 123.3 | 119 | 37 | t | n | -0.3 | n | -0.09 |
| 72 | 38.34 | 125.8 | 65 | 37 | t | n | -0.3 | n | -0.09 |
| 73 | 38.41 | 126.0 | 91 | 46 | t | n | -0.3 | n | -0.09 |
| 74 | 38.43 | 126.1 | 291 | 70 | t | n | -0.3 | n | -0.09 |
| 75 | 38.49 | 126.3 | 102 | 50 | t | n | -0.3 | n | -0.09 |
| 76 | 38.98 | 127.9 | 133 | 33 | t | n | -0.3 | n | -0.09 |
| 77 | 39.63 | 130.0 | 292 | 72 | t | n | -0.3 | n | -0.09 |
| 78 | 40.03 | 131.4 | 117 | 51 | t | n | -0.3 | n | -0.09 |
| 79 | 41.36 | 135.7 | 314 | 71 | t | n | -0.3 | n | -0.09 |
| 80 | 41.65 | 136.6 | 324 | 70 | t | n | -0.3 | n | -0.09 |
| 81 | 42.10 | 138.1 | 313 | 76 | t | n | -0.3 | n | -0.09 |
| 82 | 42.34 | 138.9 | 324 | 66 | t | n | -0.3 | n | -0.09 |
| 83 | 42.62 | 139.8 | 331 | 75 | t | n | -0.3 | n | -0.09 |
| 84 | 43.32 | 142.1 | 322 | 76 | t | n | -0.3 | n | -0.09 |
| 85 | 43.84 | 143.8 | 324 | 70 | t | n | -0.3 | n | -0.09 |
| 86 | 44.67 | 146.6 | 345 | 68 | t | n | -0.3 | n | -0.09 |
| 87 | 46.60 | 152.9 | 74 | 55 | t | n | -0.3 | n | -0.09 |
| 88 | 47.25 | 155.0 | 114 | 61 | t | n | -0.3 | n | -0.09 |
| 89 | 47.78 | 156.8 | 106 | 60 | t | n | -0.3 | n | -0.09 |
| 90 | 48.75 | 159.9 | 101 | 70 | t | n | -0.3 | n | -0.09 |
| 91 | 49.10 | 161.1 | 79 | 67 | t | n | -0.3 | n | -0.09 |
| 92 | 49.31 | 161.8 | 97 | 61 | t | n | -0.3 | n | -0.09 |
| 93 | 49.42 | 162.2 | 103 | 67 | t | n | -0.3 | n | -0.09 |
| 94 | 50.46 | 165.6 | 57 | 69 | t | n | -0.3 | n | -0.09 |
| 95 | 50.77 | 166.6 | 77 | 59 | t | n | -0.3 | n | -0.09 |
| 96 | 51.15 | 167.8 | 11 | 71 | t | n | -0.3 | n | -0.09 |
| 97 | 51.44 | 168.8 | 33 | 64 | t | n | -0.3 | n | -0.09 |
| 98 | 51.67 | 169.5 | 27 | 65 | t | n | -0.3 | n | -0.09 |
| 99 | 52.10 | 171.0 | 26 | 63 | t | n | -0.3 | n | -0.09 |
| 100 | 52.29 | 171.6 | 11 | 67 | t | n | -0.3 | n | -0.09 |
| 101 | 53.02 | 174.0 | 352 | 66 | t | n | -0.3 | n | -0.09 |
| 102 | 53.31 | 174.9 | 351 | 70 | t | n | -0.3 | n | -0.09 |
| 103 | 53.86 | 176.7 | 349 | 74 | t | n | -0.3 | n | -0.09 |
| 104 | 55.13 | 180.9 | 323 | 74 | t | n | -0.3 | n | -0.09 |
| 105 | 55.69 | 182.7 | 349 | 66 | t | n | -0.3 | n | -0.09 |
| 106 | 56.53 | 185.5 | 289 | 23 | s | n | -0.3 | n | -0.09 |
| 107 | 56.67 | 186.0 | 132 | 76 | t | n | -0.3 | n | -0.09 |
| 108 | 57.10 | 187.3 | 154 | 59 | t | n | -0.3 | n | -0.09 |
| 109 | 57.37 | 188.2 | 351 | 42 | t | n | -0.3 | n | -0.09 |
| 110 | 57.68 | 189.3 | 180 | 46 | p | n | -0.3 | n | -0.09 |
| 111 | 57.91 | 190.0 | 160 | 43 | t | n | -0.3 | n | -0.09 |
| 112 | 58.17 | 190.8 | 331 | 70 | t | n | -0.3 | n | -0.09 |
| 113 | 58.27 | 191.2 | 181 | 37 | p | n | -0.3 | n | -0.09 |
| 114 | 58.53 | 192.0 | 205 | 43 | p | n | -0.3 | n | -0.09 |

Appendix 6, continued. Midpoint depth, strike and dip of features identified in optical televiewer log, fracture type and heat pulse flowmeter data from Gates 1 (azimuth and dip reported using right hand rule convention; t = tectonic fractures, s = sheeting joints, p = foliation parallel fractures). Flow data shown under pumping conditions have been normalized.

| | | | | | | | | | | | |
|-----|-------|-------|-----|----|---|---|------|----------|-------|------|----------|
| 115 | 58.83 | 193.0 | 2 | 26 | t | n | -0.3 | n | -0.09 | | |
| 116 | 59.12 | 194.0 | 330 | 33 | t | n | -0.3 | n | -0.09 | | |
| 117 | 65.19 | 213.9 | 291 | 58 | t | n | -0.3 | n | -0.09 | | |
| 118 | 66.36 | 217.7 | 22 | 17 | s | n | -0.3 | n | -0.09 | | |
| 119 | 66.64 | 218.6 | 285 | 62 | t | n | -0.3 | n | -0.09 | | |
| 120 | 69.40 | 227.7 | 262 | 52 | p | n | -0.3 | n | -0.09 | | |
| 121 | 72.44 | 237.7 | 92 | 35 | t | n | -0.3 | n | -0.09 | | |
| 122 | 73.24 | 240.3 | 270 | 0 | s | n | -0.3 | n | -0.09 | | |
| 123 | 73.70 | 241.8 | 222 | 21 | s | y | 0 | flow out | y | 0.00 | flow out |
| 124 | 73.75 | 242.0 | 83 | 60 | t | n | 0 | n | 0.01 | | |
| 125 | 74.67 | 245.0 | 270 | 0 | s | n | 0 | n | 0.01 | | |
| 126 | 74.79 | 245.4 | 75 | 64 | t | n | 0 | n | 0.01 | | |
| 127 | 75.45 | 247.5 | 241 | 17 | s | n | 0 | n | 0.01 | | |
| 128 | 75.50 | 247.7 | 71 | 50 | t | n | 0 | n | 0.01 | | |
| 129 | 75.71 | 248.4 | 79 | 37 | t | n | 0 | n | 0.01 | | |
| 130 | 75.98 | 249.3 | 235 | 60 | p | n | 0 | n | 0.01 | | |
| 131 | 76.24 | 250.2 | 137 | 9 | s | n | 0 | n | 0.01 | | |
| 132 | 76.35 | 250.5 | 206 | 41 | p | n | 0 | n | 0.01 | | |
| 133 | 76.69 | 251.6 | 52 | 34 | t | n | 0 | n | 0.01 | | |
| 134 | 76.86 | 252.2 | 33 | 66 | t | n | 0 | n | 0.01 | | |
| 135 | 77.09 | 252.9 | 78 | 62 | t | n | 0 | n | 0.01 | | |
| 136 | 77.17 | 253.2 | 30 | 66 | t | n | 0 | n | 0.01 | | |
| 137 | 77.46 | 254.1 | 114 | 60 | t | n | 0 | n | 0.01 | | |
| 138 | 77.62 | 254.7 | 14 | 60 | t | n | 0 | n | 0.01 | | |
| 139 | 77.73 | 255.0 | 72 | 53 | t | n | 0 | n | 0.01 | | |
| 140 | 77.78 | 255.2 | 251 | 57 | p | n | 0 | n | 0.01 | | |
| 141 | 78.24 | 256.7 | 7 | 70 | t | n | 0 | n | 0.01 | | |
| 142 | 78.39 | 257.2 | 58 | 39 | t | n | 0 | n | 0.01 | | |
| 143 | 78.97 | 259.1 | 63 | 67 | t | n | 0 | n | 0.01 | | |
| 144 | 79.36 | 260.4 | 87 | 55 | t | n | 0 | n | 0.01 | | |
| 145 | 79.42 | 260.6 | 74 | 63 | t | n | 0 | n | 0.01 | | |
| 146 | 79.95 | 262.3 | 73 | 47 | t | n | 0 | n | 0.01 | | |
| 147 | 80.10 | 262.8 | 67 | 65 | t | n | 0 | n | 0.01 | | |
| 148 | 80.69 | 264.8 | 322 | 35 | t | n | 0 | n | 0.01 | | |
| 149 | 81.12 | 266.2 | 253 | 65 | p | n | 0 | n | 0.01 | | |
| 150 | 81.23 | 266.5 | 85 | 46 | t | n | 0 | n | 0.01 | | |
| 151 | 81.88 | 268.6 | 90 | 49 | t | n | 0 | n | 0.01 | | |
| 152 | 82.18 | 269.6 | 93 | 53 | t | n | 0 | n | 0.01 | | |
| 153 | 82.52 | 270.8 | 84 | 56 | t | n | 0 | n | 0.01 | | |
| 154 | 82.97 | 272.2 | 103 | 43 | t | n | 0 | n | 0.01 | | |
| 155 | 83.87 | 275.2 | 275 | 51 | t | n | 0 | n | 0.01 | | |
| 156 | 83.98 | 275.5 | 186 | 7 | s | n | 0 | n | 0.01 | | |
| 157 | 84.18 | 276.2 | 247 | 44 | p | n | 0 | n | 0.01 | | |
| 158 | 84.93 | 278.7 | 284 | 63 | t | n | 0 | n | 0.01 | | |
| 159 | 87.07 | 285.7 | 254 | 47 | p | n | 0 | n | 0.01 | | |
| 160 | 87.50 | 287.1 | 223 | 39 | p | n | 0 | n | 0.01 | | |
| 161 | 87.81 | 288.1 | 258 | 36 | p | n | 0 | n | 0.01 | | |
| 162 | 88.53 | 290.5 | 165 | 49 | p | n | 0 | n | 0.01 | | |
| 163 | 88.89 | 291.6 | 90 | 72 | t | n | 0 | n | 0.01 | | |
| 164 | 89.16 | 292.5 | 90 | 60 | t | n | 0 | n | 0.01 | | |
| 165 | 89.57 | 293.9 | 277 | 68 | t | n | 0 | n | 0.01 | | |
| 166 | 89.85 | 294.8 | 240 | 57 | p | n | 0 | n | 0.01 | | |
| 167 | 90.09 | 295.6 | 242 | 36 | p | n | 0 | n | 0.01 | | |
| 168 | 90.77 | 297.8 | 86 | 51 | t | n | 0 | n | 0.01 | | |
| 169 | 92.21 | 302.5 | 263 | 78 | t | n | 0 | n | 0.01 | | |
| 170 | 92.43 | 303.3 | 270 | 73 | t | n | 0 | n | 0.01 | | |
| 171 | 93.30 | 306.1 | 120 | 38 | t | n | 0 | n | 0.01 | | |
| 172 | 94.05 | 308.6 | 78 | 29 | t | n | 0 | n | 0.01 | | |
| 173 | 96.76 | 317.5 | 277 | 49 | t | n | 0 | n | 0.01 | | |
| 174 | 98.16 | 322.1 | 60 | 29 | t | n | 0 | n | 0.01 | | |
| 175 | 98.88 | 324.4 | 257 | 74 | p | n | 0 | n | 0.01 | | |
| 176 | 99.32 | 325.9 | 73 | 42 | t | n | 0 | n | 0.01 | | |
| 177 | 99.59 | 326.8 | 64 | 53 | t | n | 0 | n | 0.01 | | |
| 178 | 99.63 | 326.9 | 242 | 78 | p | n | 0 | n | 0.01 | | |

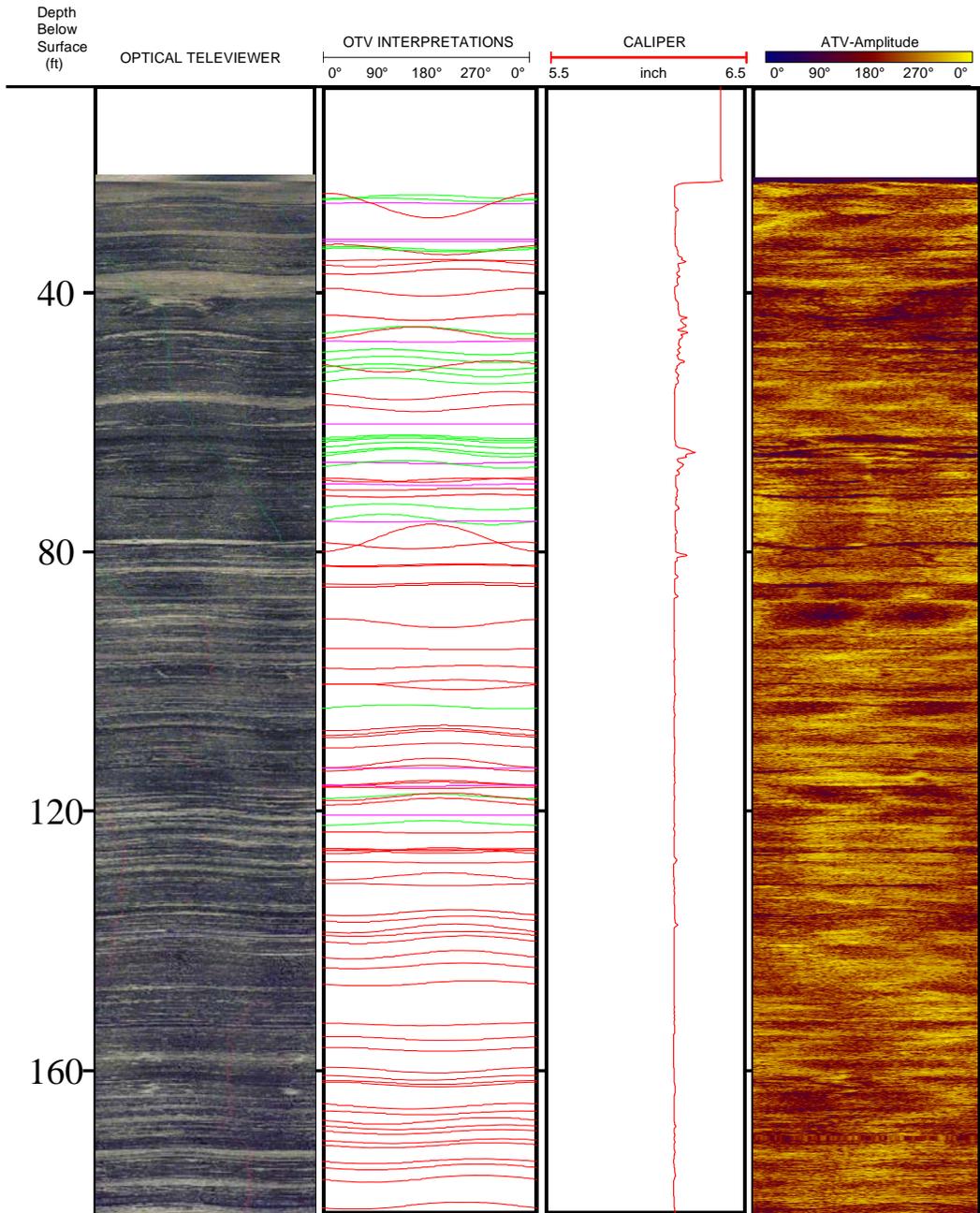
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| | | | | | | | | | |
|-----|--------|-------|-----|----|---|---|---|---|--------------|
| 179 | 101.82 | 334.1 | 234 | 75 | p | n | 0 | n | 0.01 |
| 180 | 102.47 | 336.2 | 232 | 73 | p | n | 0 | n | 0.01 |
| 181 | 103.85 | 340.7 | 239 | 61 | p | n | 0 | n | 0.01 |
| 182 | 104.33 | 342.3 | 49 | 59 | t | n | 0 | n | 0.01 |
| 183 | 104.66 | 343.4 | 62 | 54 | t | n | 0 | n | 0.01 |
| 184 | 106.40 | 349.1 | 211 | 76 | p | n | 0 | y | 0.01 flow in |
| 185 | 110.84 | 363.7 | 42 | 37 | t | n | 0 | n | 0.00 |
| 186 | 111.48 | 365.8 | 204 | 75 | p | n | 0 | n | 0.00 |
| 187 | 111.65 | 366.3 | 51 | 34 | t | n | 0 | n | 0.00 |
| 188 | 112.47 | 369.0 | 315 | 10 | s | n | 0 | n | 0.00 |
| 189 | 112.79 | 370.1 | 207 | 73 | p | n | 0 | n | 0.00 |
| 190 | 114.68 | 376.3 | 234 | 28 | p | n | 0 | n | 0.00 |
| 191 | 114.91 | 377.0 | 340 | 29 | t | n | 0 | n | 0.00 |
| 192 | 115.06 | 377.5 | 14 | 42 | t | n | 0 | n | 0.00 |
| 193 | 116.35 | 381.8 | 213 | 70 | p | n | 0 | n | 0.00 |
| 194 | 116.85 | 383.4 | 269 | 28 | p | n | 0 | n | 0.00 |
| 195 | 117.03 | 384.0 | 244 | 62 | p | n | 0 | n | 0.00 |
| 196 | 117.47 | 385.4 | 327 | 21 | s | n | 0 | n | 0.00 |
| 197 | 118.15 | 387.7 | 286 | 35 | p | n | 0 | n | 0.00 |
| 198 | 118.67 | 389.4 | 346 | 32 | t | n | 0 | n | 0.00 |
| 199 | 118.81 | 389.8 | 329 | 41 | t | n | 0 | n | 0.00 |
| 200 | 118.99 | 390.4 | 35 | 31 | t | n | 0 | n | 0.00 |
| 201 | 119.23 | 391.2 | 301 | 22 | s | n | 0 | n | 0.00 |
| 202 | 120.02 | 393.8 | 304 | 44 | t | n | 0 | n | 0.00 |
| 203 | 120.10 | 394.1 | 335 | 24 | s | n | 0 | n | 0.00 |
| 204 | 120.57 | 395.6 | 267 | 21 | s | n | 0 | n | 0.00 |
| 205 | 121.21 | 397.7 | 5 | 25 | s | n | 0 | n | 0.00 |
| 206 | 121.80 | 399.6 | 261 | 23 | s | n | 0 | n | 0.00 |
| 207 | 121.93 | 400.0 | 173 | 18 | s | n | 0 | n | 0.00 |
| 208 | 122.58 | 402.2 | 136 | 16 | s | n | 0 | n | 0.00 |
| 209 | 123.58 | 405.5 | 279 | 58 | t | n | 0 | n | 0.00 |
| 210 | 124.04 | 407.0 | 296 | 59 | t | n | 0 | n | 0.00 |
| 211 | 124.53 | 408.6 | 182 | 64 | p | n | 0 | n | 0.00 |
| 212 | 124.67 | 409.0 | 260 | 12 | s | n | 0 | n | 0.00 |
| 213 | 125.12 | 410.5 | 169 | 76 | t | n | 0 | n | 0.00 |
| 214 | 125.28 | 411.0 | 275 | 54 | t | n | 0 | n | 0.00 |
| 215 | 125.54 | 411.9 | 164 | 65 | t | n | 0 | n | 0.00 |
| 216 | 125.71 | 412.4 | 28 | 8 | s | n | 0 | n | 0.00 |
| 217 | 125.92 | 413.2 | 105 | 72 | t | n | 0 | n | 0.00 |
| 218 | 126.26 | 414.3 | 159 | 81 | t | n | 0 | n | 0.00 |
| 219 | 126.64 | 415.5 | 183 | 67 | p | n | 0 | n | 0.00 |
| 220 | 126.82 | 416.1 | 160 | 48 | t | n | 0 | n | 0.00 |
| 221 | 127.21 | 417.4 | 224 | 56 | t | n | 0 | n | 0.00 |
| 222 | 127.99 | 420.0 | 130 | 73 | t | n | 0 | n | 0.00 |
| 223 | 128.52 | 421.7 | 158 | 66 | t | n | 0 | n | 0.00 |
| 224 | 129.54 | 425.0 | 171 | 43 | p | n | 0 | n | 0.00 |
| 225 | 130.45 | 428.0 | 199 | 42 | p | n | 0 | n | 0.00 |
| 226 | 131.55 | 431.6 | 313 | 77 | t | n | 0 | n | 0.00 |
| 227 | 131.88 | 432.7 | 15 | 74 | t | n | 0 | n | 0.00 |
| 228 | 132.43 | 434.5 | 173 | 69 | t | n | 0 | n | 0.00 |
| 229 | 132.70 | 435.4 | 173 | 77 | t | n | 0 | n | 0.00 |
| 230 | 132.93 | 436.1 | 166 | 77 | t | n | 0 | n | 0.00 |
| 231 | 133.86 | 439.2 | 182 | 66 | p | n | 0 | n | 0.00 |
| 232 | 134.55 | 441.5 | 164 | 67 | t | n | 0 | n | 0.00 |
| 233 | 134.79 | 442.2 | 188 | 66 | p | n | 0 | n | 0.00 |
| 234 | 136.73 | 448.6 | 196 | 69 | t | n | 0 | n | 0.00 |
| 235 | 137.54 | 451.3 | 172 | 70 | t | n | 0 | n | 0.00 |
| 236 | 138.42 | 454.2 | 180 | 69 | p | n | 0 | n | 0.00 |
| 237 | 139.95 | 459.2 | 317 | 68 | t | n | 0 | n | 0.00 |
| 238 | 140.16 | 459.9 | 318 | 75 | t | n | 0 | n | 0.00 |
| 239 | 140.70 | 461.6 | 231 | 51 | p | n | 0 | n | 0.00 |
| 240 | 145.29 | 476.7 | 267 | 69 | p | n | 0 | n | 0.00 |
| 241 | 148.22 | 486.3 | 269 | 58 | t | n | 0 | n | 0.00 |
| 242 | 149.36 | 490.1 | 286 | 42 | t | n | 0 | n | 0.00 |

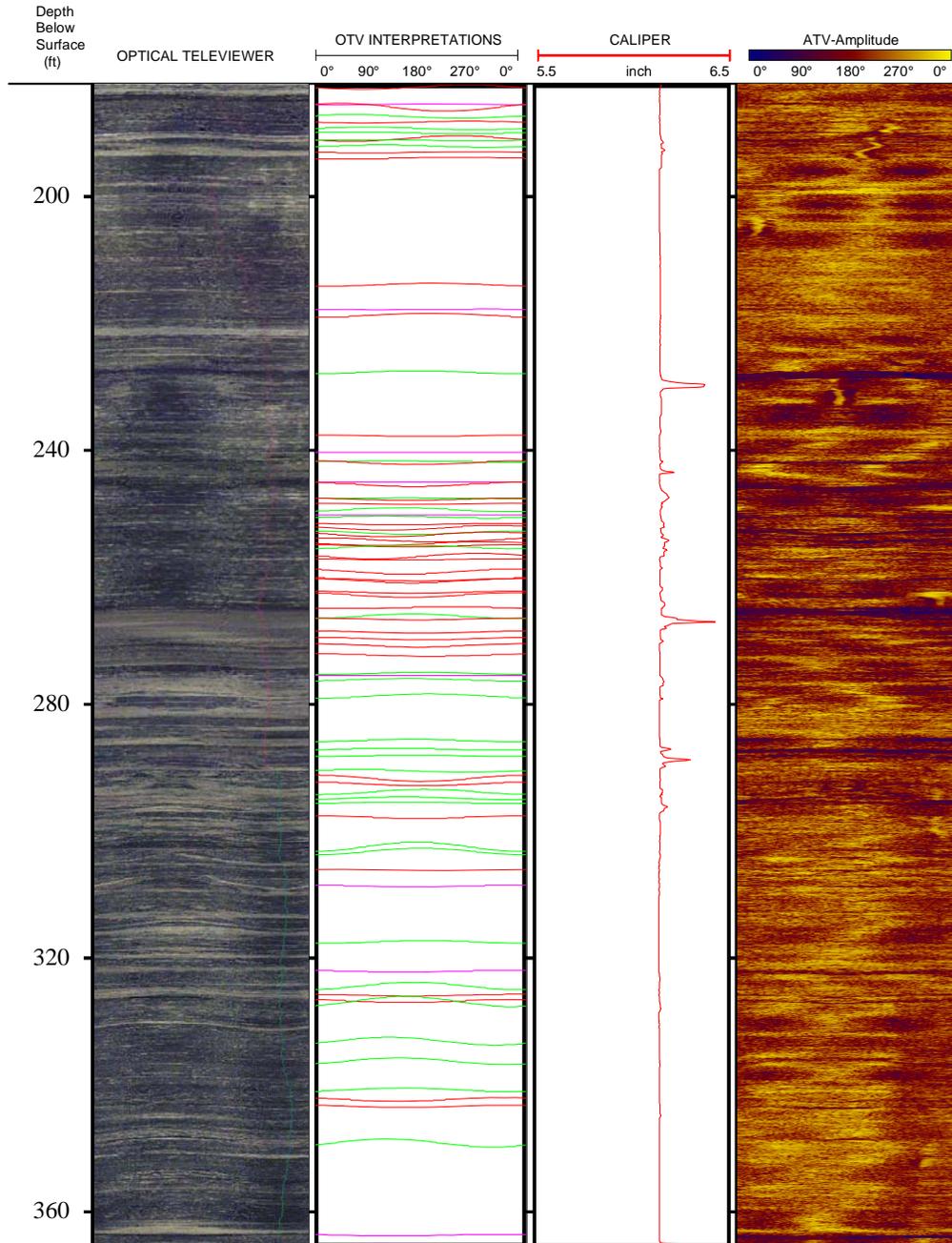
Appendix 6, continued. Midpoint depth, strike and dip of features identified in optical televiewer log, fracture type and heat pulse flowmeter data from Gates 1 (azimuth and dip reported using right hand rule convention; t = tectonic fractures, s = sheeting joints, p = foliation parallel fractures). Flow data under pumping conditions have been normalized.

| | | | | | | | | | |
|-----|--------|-------|-----|----|---|---|---|---|------|
| 243 | 149.47 | 490.4 | 285 | 44 | t | n | 0 | n | 0.00 |
| 244 | 150.03 | 492.2 | 273 | 63 | t | n | 0 | n | 0.00 |
| 245 | 151.16 | 496.0 | 303 | 53 | t | n | 0 | n | 0.00 |
| 246 | 154.89 | 508.2 | 264 | 71 | t | n | 0 | n | 0.00 |
| 247 | 155.31 | 509.6 | 276 | 70 | t | n | 0 | n | 0.00 |
| 248 | 157.01 | 515.1 | 257 | 64 | p | n | 0 | n | 0.00 |
| 249 | 157.38 | 516.4 | 275 | 58 | t | n | 0 | n | 0.00 |
| 250 | 161.06 | 528.4 | 273 | 69 | t | n | 0 | n | 0.00 |
| 251 | 161.37 | 529.4 | 80 | 75 | t | n | 0 | n | 0.00 |
| 252 | 161.91 | 531.2 | 263 | 52 | p | n | 0 | n | 0.00 |
| 253 | 163.30 | 535.8 | 326 | 86 | t | n | 0 | n | 0.00 |
| 254 | 163.75 | 537.3 | 148 | 76 | t | n | 0 | n | 0.00 |
| 255 | 166.32 | 545.7 | 218 | 54 | p | n | 0 | n | 0.00 |

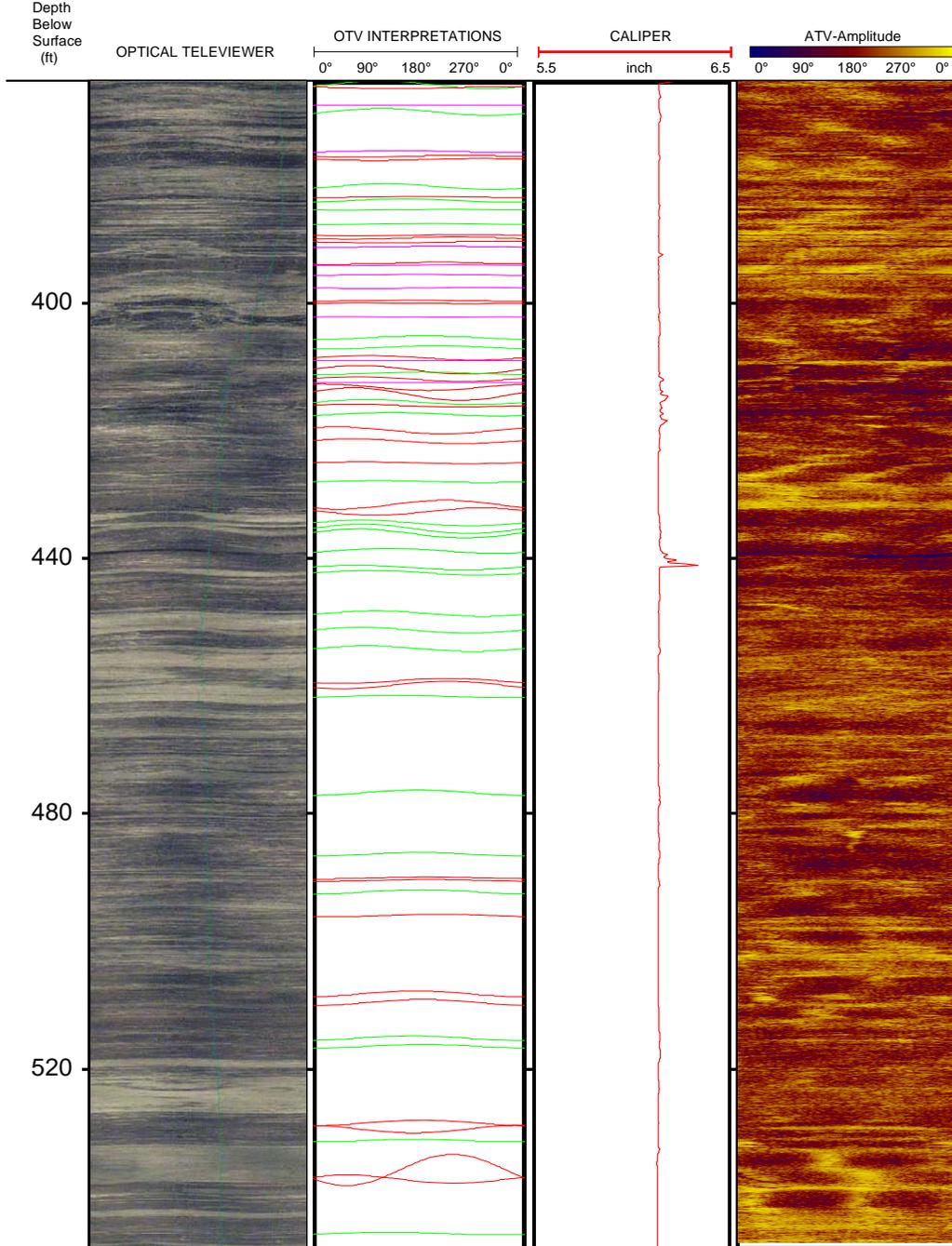
Appendix 6, continued. Interpreted features for Gates 1. Optical televiewer interpretations indicated by color: orange – subhorizontal sheeting joint; magenta – tectonic joint; red – foliation parallel fracture (FPF); cyan – transmissive subhorizontal sheeting joint; green – transmissive tectonic joint; grey – transmissive foliation parallel fracture (FPF). OTV – optical televiewer; ATV – acoustic televiewer.



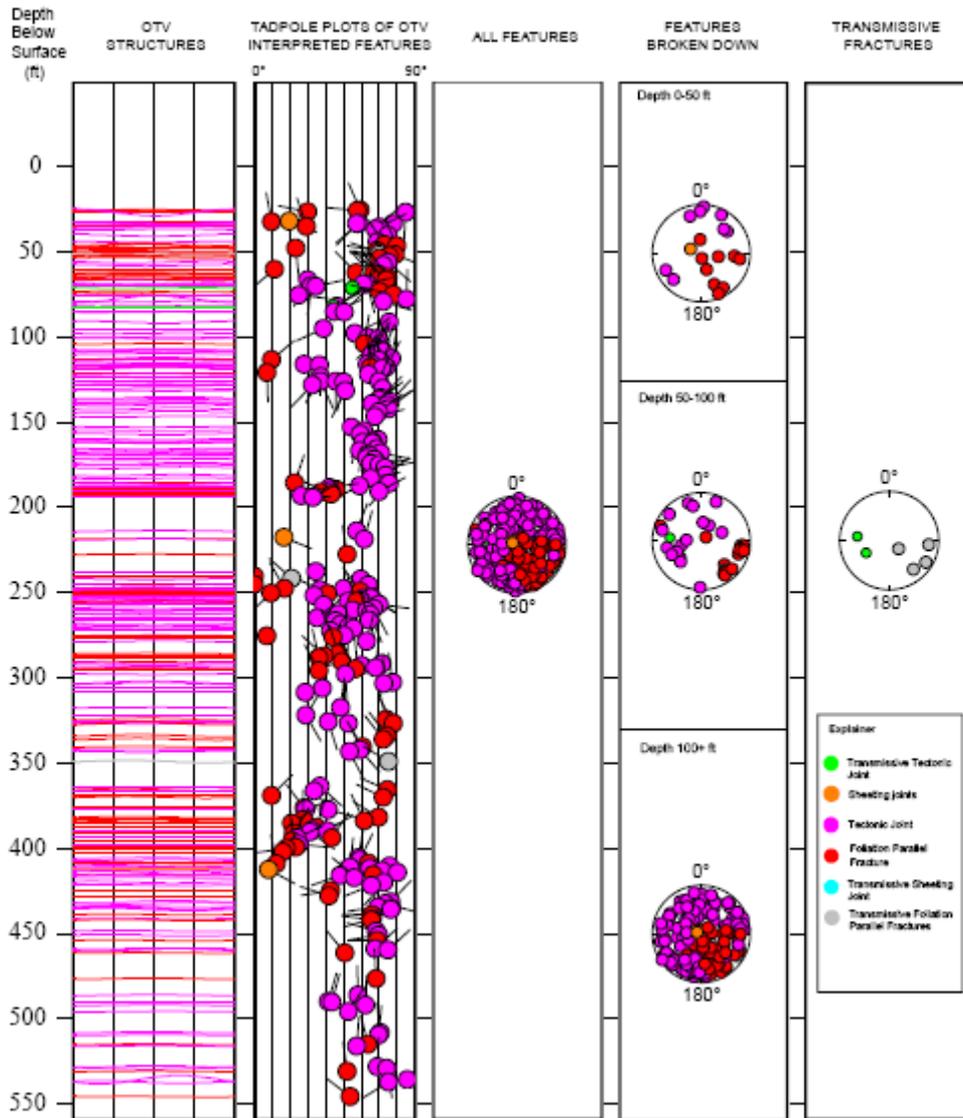
Appendix 6, continued. Interpreted features for Gates 1. Optical televiewer interpretations indicated by color: orange – subhorizontal sheeting joint; magenta – tectonic joint; red – foliation parallel fracture (FPF); cyan – transmissive subhorizontal sheeting joint; green – transmissive tectonic joint; grey – transmissive foliation parallel fracture (FPF). OTV – optical televiewer; ATV – acoustic televiewer.



Appendix 6, continued. Interpreted features for Gates 1. Optical televiewer interpretations indicated by color: orange – subhorizontal sheeting joint; magenta – tectonic joint; red – foliation parallel fracture (FPF); cyan – transmissive subhorizontal sheeting joint; green – transmissive tectonic joint; grey – transmissive foliation parallel fracture (FPF). OTV – optical televiewer; ATV – acoustic televiewer.



Appendix 6, continued. Tadpole plots and stereoplots of interpreted optical televiwer (OTV) structures for Gates 1. In the tadpole plot depth is plotted along the y-axis and magnitude of the dip plotted on the x-axis. The tail of the tadpole points in the direction of the dip, relative to true north, which is toward the top of the page. The stereonets represent poles to planar features plotted on a lower-hemisphere equal-area stereonet. Stereonets use right hand rule convention. Colors on the OTV structures plot correspond to those in the tadpole explanation.



Appendix 6, continued. Composite log for Gates 1 of natural gamma, fluid resistivity, fluid temperature and heat pulse flowmeter data under ambient and stressed (pumping) conditions. For the heat pulse flowmeter data collected under pumping conditions, the well was pumped at 0.5 gallons per minute and the data have been normalized.

